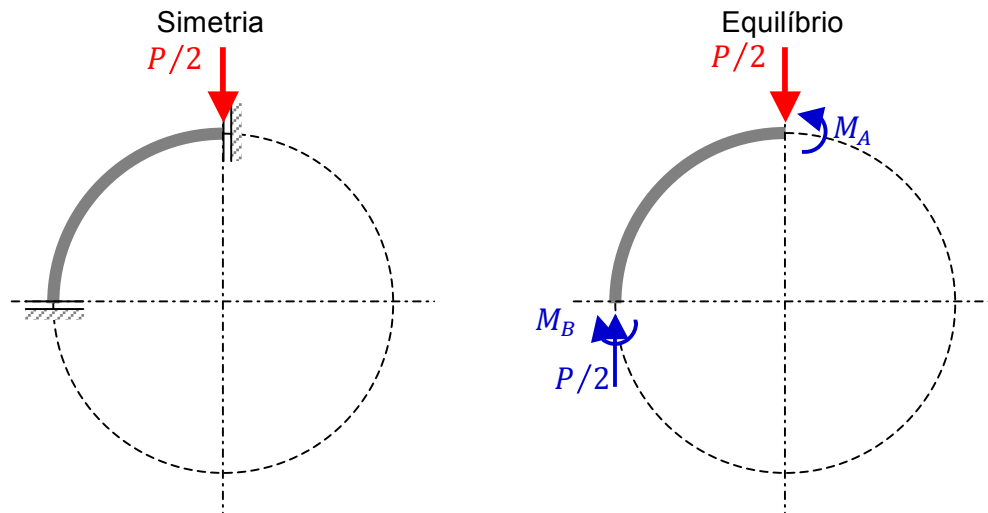
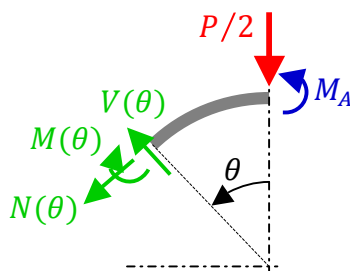


Problema 1. (3,5 pontos)



Distribuição do Momento Fletor



$$M(\theta) = M_A - \frac{P}{2} R \sin \theta, \quad 0 < \theta < \pi/2$$

$$\frac{\partial M}{\partial M_A} = 1$$

$$\phi_A = \frac{\partial U}{\partial M_A} = 0$$

logo

$$\frac{\partial U}{\partial M_A} = \frac{1}{EI} \int_0^{\pi/2} M(\theta) \frac{\partial M}{\partial M_A} R d\theta = \frac{1}{EI} \int_0^{\pi/2} \left[M_A - \frac{P}{2} R \sin \theta \right] R d\theta = \frac{R}{EI} \left[\frac{M_A \pi}{2} - \frac{PR}{2} \right] = 0 \Rightarrow M_A = \frac{PR}{\pi}$$

$$M_B = M(\pi/2) = M_A - PR/2 = -\frac{(\pi - 2) PR}{2\pi}$$

Distribuição de tensões

$$\sigma_{\theta\theta}(y, \theta) = -y \frac{M(\theta)}{I} + \frac{N(\theta)}{A}, \quad -a/2 < y < a/2 \quad (I = a^4/12, \quad A = a^2)$$

Na Seção A ($\theta = 0$)

$$\sigma_{\theta\theta}(y, 0) = -y \frac{M_A}{I} = -12y \frac{PR}{\pi a^4}$$

$$\max\{|\sigma_{\theta\theta}(y, 0)|\} = \left| \sigma_{\theta\theta} \left(\pm \frac{a}{2}, 0 \right) \right| = \frac{6PR}{\pi a^3}$$

Na Seção B ($\theta = \pi/2$)

$$\sigma_{\theta\theta}\left(y, \frac{\pi}{2}\right) = -y \frac{M_B}{I} - \frac{P/2}{A} = 6(\pi - 2)y \frac{PR}{\pi a^4} - \frac{P}{2a^2}$$

$$\max\{|\sigma_{\theta\theta}(y, \pi/2)|\} = \left|\sigma_{\theta\theta}\left(-\frac{a}{2}, 0\right)\right| = \left[\frac{(\pi - 2)}{2} + \frac{\pi}{12} \frac{a}{R}\right] \frac{6PR}{\pi a^3}$$

Para vigas curvas esbeltas $a/R \ll 1$ e, portanto, $[(\pi - 2)/2 + \pi(a/R)/12] < 1$. Nesse caso, a máxima tensão de flexão, em valor absoluto, ocorre na Seção A.

Problema 2 (3,0 pontos).

Compatibilidade de deformações

$$\frac{(P - R_1)L^3}{3EI} = \frac{(R_1 - R_2)L^3}{3EI} = \frac{R_2(3L)}{EA}$$

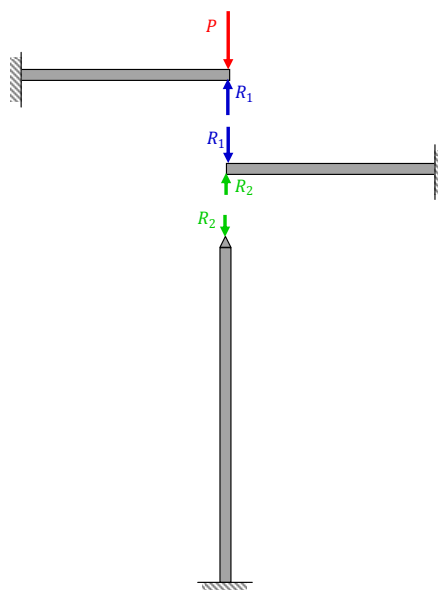
Logo

$$P - R_1 = R_1 - R_2 = 9 \left(\frac{I/A}{L^2} \right) R_2$$

$$R_2 = \frac{P}{1 + 18\xi}, \text{ onde } \xi = \frac{I/A}{L^2}$$

$$R_2 < \frac{\pi^2}{4} \frac{EI}{(3L)^2} \Rightarrow P < (1 + 18\xi) \frac{\pi^2}{4} \frac{EI}{9L^2} = 8,2 \text{ kN}$$

$$P < 8,2 \text{ kN}$$



Problema 3 (3,5 pontos)

$$\delta_A = \frac{\partial U}{\partial P} = \frac{1}{EI} \int M \frac{\partial M}{\partial P} ds + \frac{1}{GJ} \int T \frac{\partial T}{\partial P} ds$$

(a) Trecho paralelo à direção z ($0 < z < L$)

$$M_y(z) = -Pz \quad \partial M_y / \partial P = -z$$

$$M_x(z) = 0$$

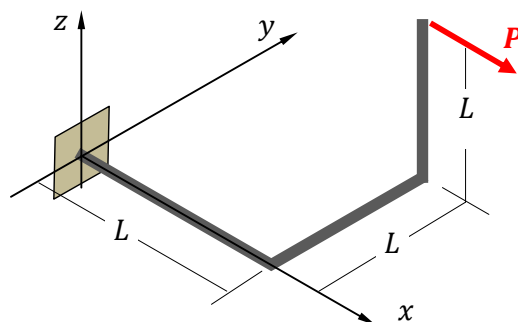
$$T(z) = M_z(z) = 0$$

(b) Trecho paralelo à direção y ($0 < y < L$)

$$M_z(y) = -Py \quad \partial M_z / \partial P = -y$$

$$M_x(y) = 0$$

$$T(y) = M_z(y) = PL \quad \partial T / \partial P = L$$



(c) Trecho paralelo à direção x ($0 < x < L$)

$$M_z(x) = -PL \quad \partial M_z / \partial P = -L$$

$$M_y(x) = PL \quad \partial M_y / \partial P = L$$

$$T(x) = M_x(x) = 0$$

$$\delta_A = \frac{1}{EI} \left[\int_0^L (-Pz)(-z) dz + \int_0^L (-Py)(-y) dy + \int_0^L (-PL)(-L) dx + \int_0^L (PL)(L) dx \right] + \frac{1}{GJ} \int_0^L (PL)(L) dy$$

$$= \frac{1}{EI} \left[\frac{PL^3}{3} + \frac{PL^3}{3} + PL^3 + PL^3 \right] + \frac{1}{GJ} PL^3$$

$$\delta_A = \frac{8PL^3}{3EI} + \frac{PL^3}{GJ} = \frac{64PL^3}{3\pi ED^4} (11 + 3\nu)$$